

**VNIIAES**

***On Development and Implementation of Normative Documentation on Evaluation  
of Technical Status and Residual Life of NPP Pipelines  
Subjected to Erosion-Corrosion Wear***

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***IAEA Technical Workshop «Erosion-corrosion wear including flow  
accelerated corrosion (FAC) and environmentally assisted cracking (EAC)  
issues at nuclear plants»  
April 21-23, 2009, Moscow, Russian Federation***

**VNIIAES, 109507, Moscow,  
Ferganskaya str., 25**

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# Developed Normative Documentation on Erosion-Corrosion Wear (E/C)

- 1. **Software** ECI-02. ECI-02 software registration and qualification certificate date is 17.03.2003, passport issued 19.09.2003.
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- 2. **Software** ECI-03. ECI-03 software registration and qualification certificate date is 17.03.2005, passport issued 23.06.2005.
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- 3. **Guidelines** «Norms of permissible thickness for pipeline elements from carbon steel at nuclear plants» RD EO 0571-2006. Put into force in 01.11.2006.
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- 4. **Methodological instruction** «Analysis of steel chemical composition by spectral and photoelectric method. Pipelines and components at power units 3&4 of Novovoronezh NPP» . 27.18.05.010-2004. Methodological instruction. Agreed by M.Miroshnichenko, Director of nuclear plant safety control department of Federal Service on environmental and nuclear inspection, 25.11.2004.

# Factors Considered by the Software Tools

- **Software tools consider erosion-corrosion influence of the following factors:**
- **water chemistry indicators (type of amine applied, water pH, oxygen content in water);**
- **parameters of mode (water velocity and temperature);**
- **content of chemical elements in pipeline metal (chromium, molybdenum and copper);**
- **pipeline geometry (inner diameter, wall thickness, Keller factor);**
- **duration of operation (start and finish of pipeline operation).**
- **steam wetness (for ECI-DS software)**

# Software Possibilities

- ECI-OS & ECI-DS software allows for:
- Data input for calculations;
- Checking correctness of data input;
- Calculations of initial, final and average rate of E/C and wall thinning for a defined time period
  - With one set of initial parameters;
  - With many sets of initial parameters (one or two variable parameters);
- Output calculation results in graphs and tables:
  - to display;
  - to printer;
  - to file;
- Adjust graphic presentation of calculation results;
- Get help working with a software.

# Dialog Box of ECI 02.1 Software

The screenshot shows a software window titled "ЭКИ-01" with a menu bar containing "Файл", "Расчет", "Настройки", and "Справка". Below the menu is a toolbar with icons for file operations and calculation. The main area is divided into two panels. The left panel, "Исходные данные", contains input fields for various parameters. The right panel, "Свойства решаемой задачи", contains a "Тип:" dropdown set to "Прямая" and a "Параметр с фиксированным шагом" dropdown menu. The dropdown menu is open, showing a list of parameters including "Содержание хрома (0 - 2 %)", "Температура воды (38 - 255 С)", "Скорость воды (0,002 - 38 м/с)", "рН воды (7 - 10,2)", "Концентрация кислорода (0 - 500 мкг/кг)", "Диаметр трубопровода (13 - 1370 мм)", "Коэффициент Келлера (0,04 - 1)", "Содержание хрома (0 - 2 %)", "Содержание молибдена (0 - 0,57 %)", "Содержание меди (0 - 0,5 %)", and "Конечный момент времени (1 - 50 лет)".

Исходные данные	
Тип амина	Аммиак
Температура воды, С	156
Скорость воды, м/с	6,1
рН воды	7
Концентрация кислорода, мкг/кг	8
Диаметр трубопровода, мм	100
Коэффициент Келлера	0,04
Содержание хрома, %	
Содержание молибдена, %	0,03
Содержание меди, %	0,03
Начальный момент времени, лет	0
Конечный момент времени, лет	15
Утонение, мм	

Свойства решаемой задачи	
Тип:	Прямая
Параметр с фиксированным шагом	
Содержание хрома (0 - 2 %)	
(Нет)	
Температура воды (38 - 255 С)	
Скорость воды (0,002 - 38 м/с)	
рН воды (7 - 10,2)	
Концентрация кислорода (0 - 500 мкг/кг)	
Диаметр трубопровода (13 - 1370 мм)	
Коэффициент Келлера (0,04 - 1)	
Содержание хрома (0 - 2 %)	
Содержание молибдена (0 - 0,57 %)	
Содержание меди (0 - 0,5 %)	
Конечный момент времени (1 - 50 лет)	

# Example of Calculations by ECI-02.1 Software

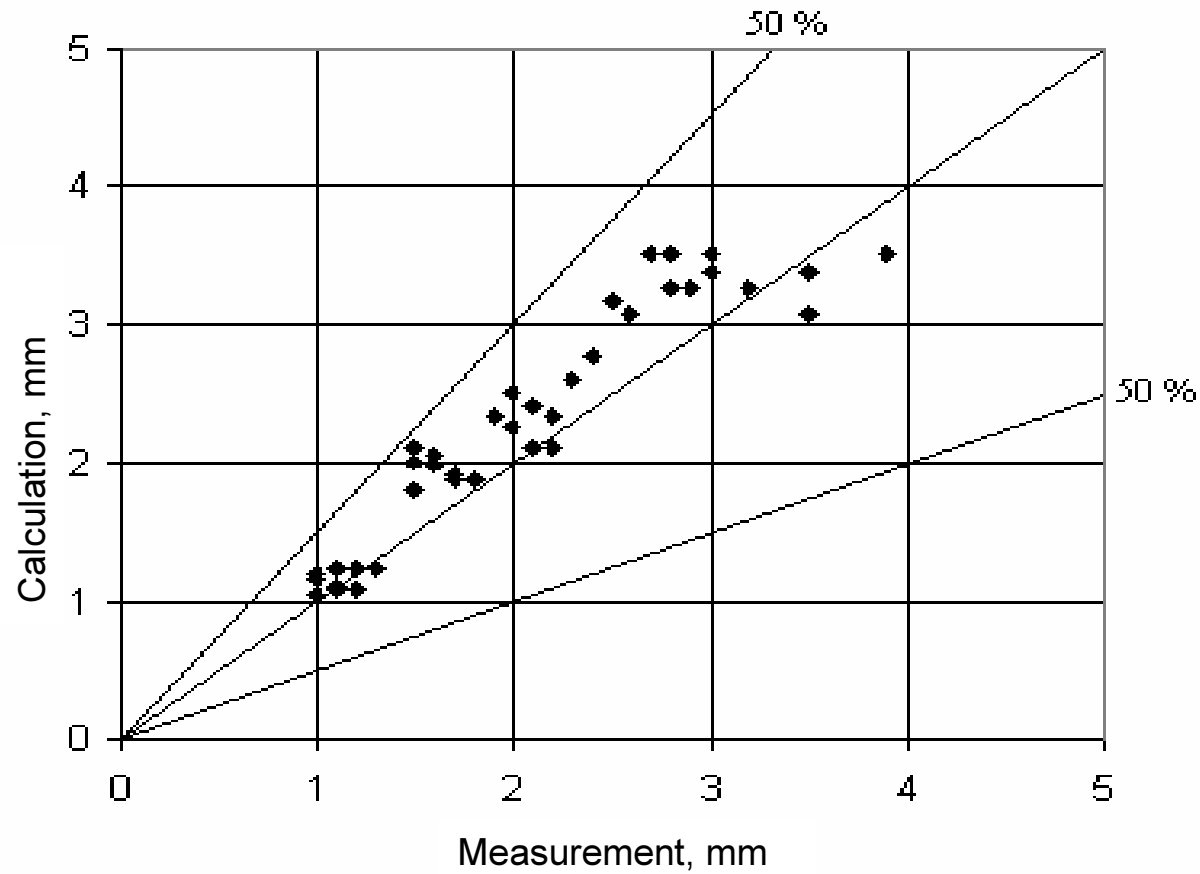
Результаты решения прямой задачи

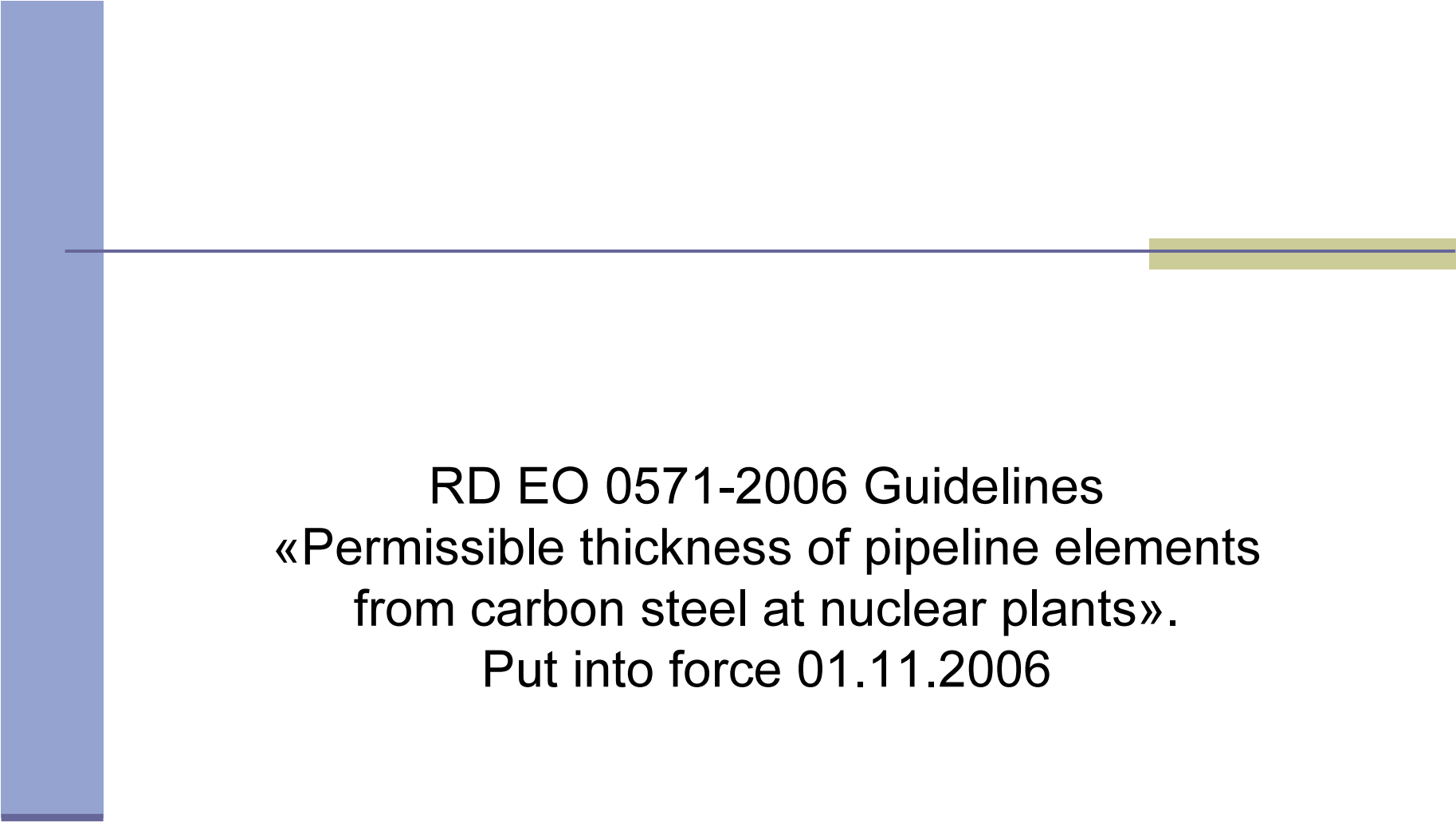
Отображаемая скорость ЭКИ или утонение  
 Начальная  Конечная  Средняя  Утонение

Исходные данные | **Полная таблица** | Краткая таблица | График

Амин	T	w	pH	O2	D	Ke	Cr	Mo	Cu	Tнач	Tкон	ЭКИ <sub>н</sub>	ЭКИ <sub>к</sub>	ЭКИ <sub>с</sub>	Утон
	С	м/с		мкг/кг	мм		%	%	%	лет	лет	мм/год	мм/год	мм/год	мм
Амми:	156	6,1	7	8	100	0,04	0	0,03	0,03	0	15	1,38	0,1841	0,3716	5,573
Амми:	156	6,1	7	8	100	0,04	0,2	0,03	0,03	0	15	0,3043	0,0405	0,0819	1,229
Амми:	156	6,1	7	8	100	0,04	0,4	0,03	0,03	0	15	0,1606	0,0214	0,0432	0,6486
Амми:	156	6,1	7	8	100	0,04	0,6	0,03	0,03	0	15	0,1103	0,0147	0,0297	0,4455
Амми:	156	6,1	7	8	100	0,04	0,8	0,03	0,03	0	15	0,0858	0,0114	0,0231	0,3468
Амми:	156	6,1	7	8	100	0,04	1	0,03	0,03	0	15	0,0713	0,0095	0,0192	0,2881
Амми:	156	6,1	7	8	100	0,04	1,2	0,03	0,03	0	15	0,0617	0,0082	0,0166	0,2495
Амми:	156	6,1	7	8	100	0,04	1,4	0,03	0,03	0	15	0,0551	0,0073	0,0148	0,2226
Амми:	156	6,1	7	8	100	0,04	1,6	0,03	0,03	0	15	0,0502	0,0067	0,0135	0,2029
Амми:	156	6,1	7	8	100	0,04	1,8	0,03	0,03	0	15	0,0466	0,0062	0,0125	0,1883
Амми:	156	6,1	7	8	100	0,04	2	0,03	0,03	0	15	0,0438	0,0058	0,0118	0,1772

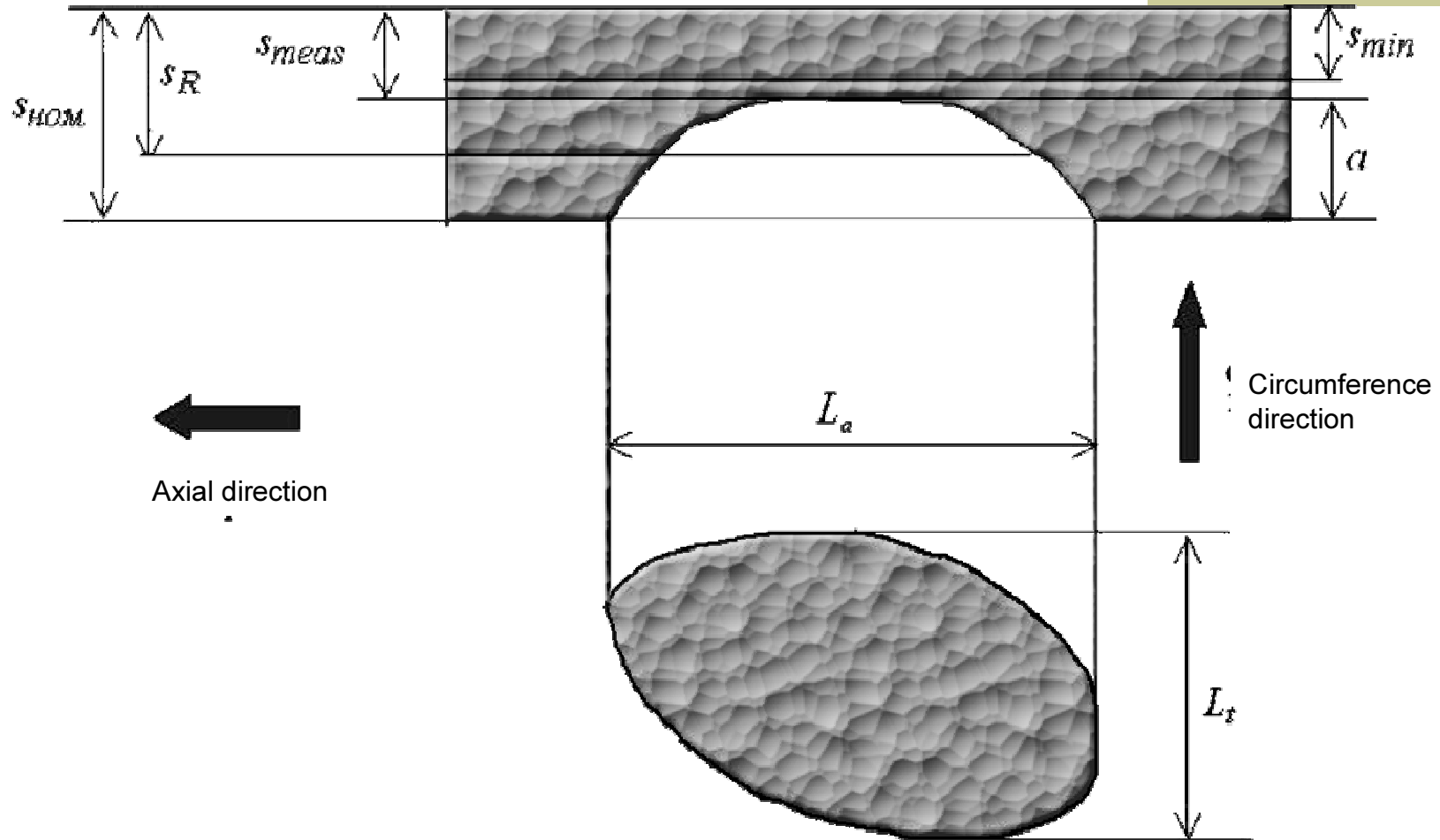
## Comparison of Calculation Results by ECI-01 Software with Operating Measurement Data of Wall Thinning in Feedwater Pipelines



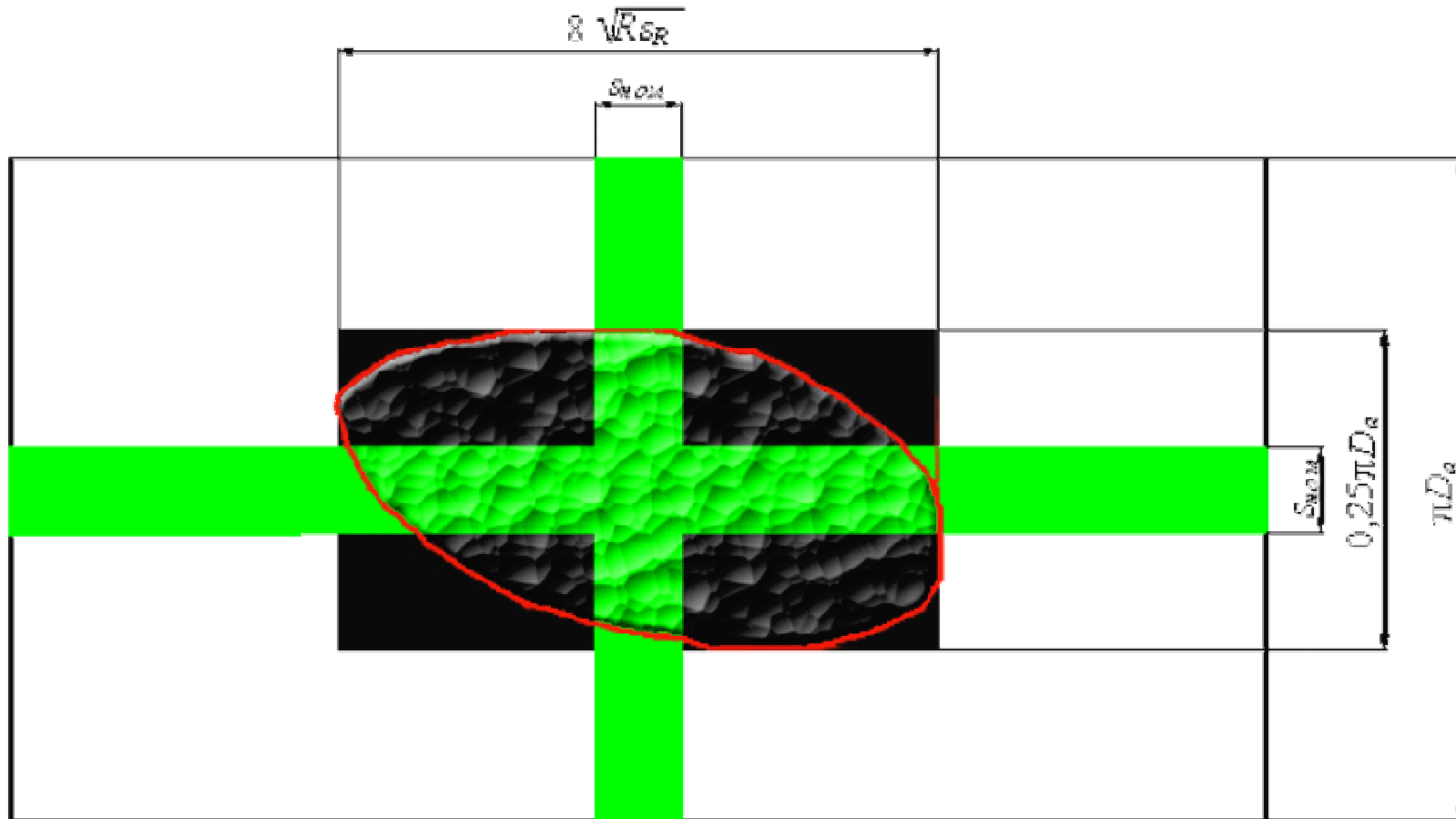


RD EO 0571-2006 Guidelines  
«Permissible thickness of pipeline elements  
from carbon steel at nuclear plants».  
Put into force 01.11.2006

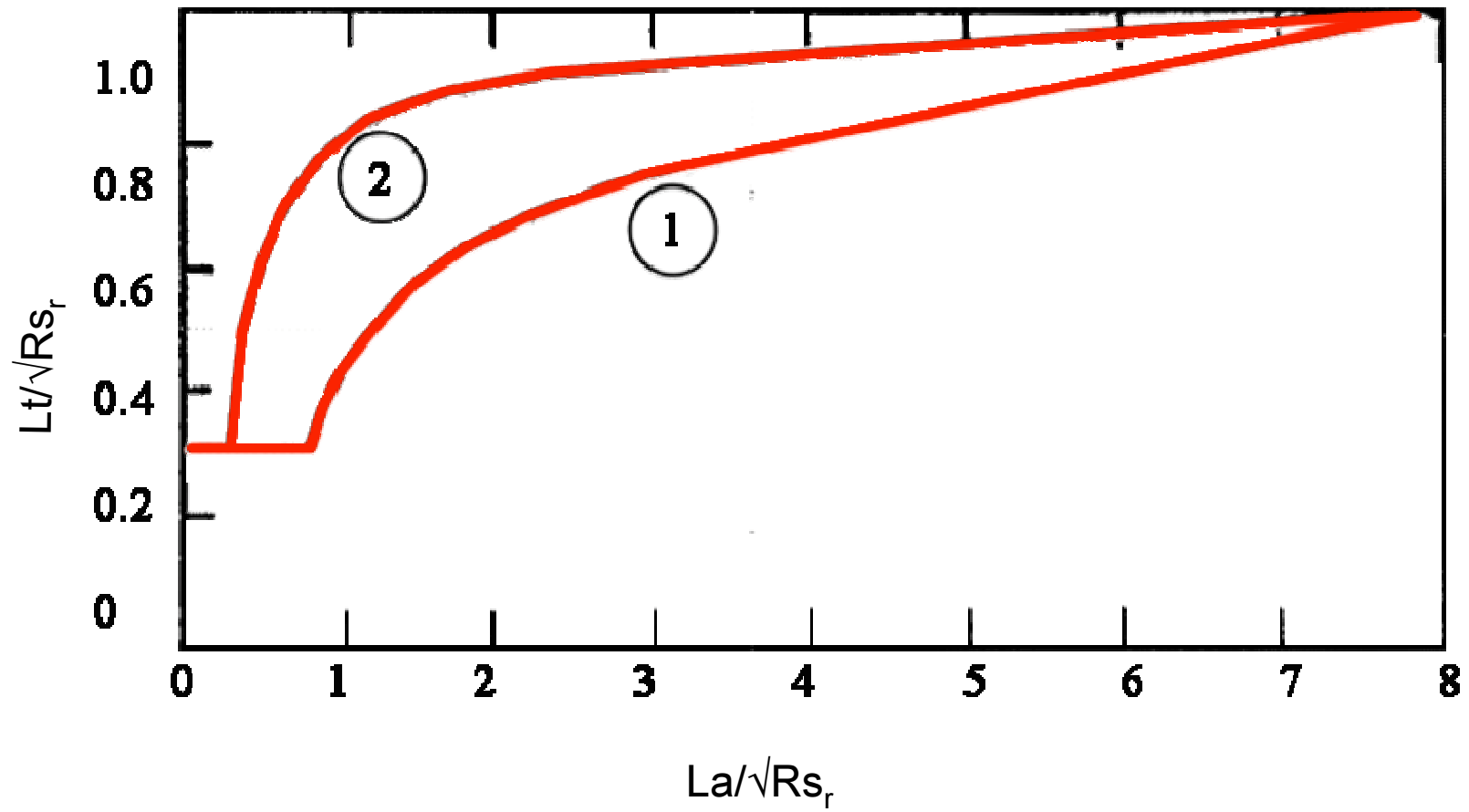
**Local Wear of Pipeline Wall with Main Dimensions**



*Scanning of Pipeline Surface Divided into Three Areas*

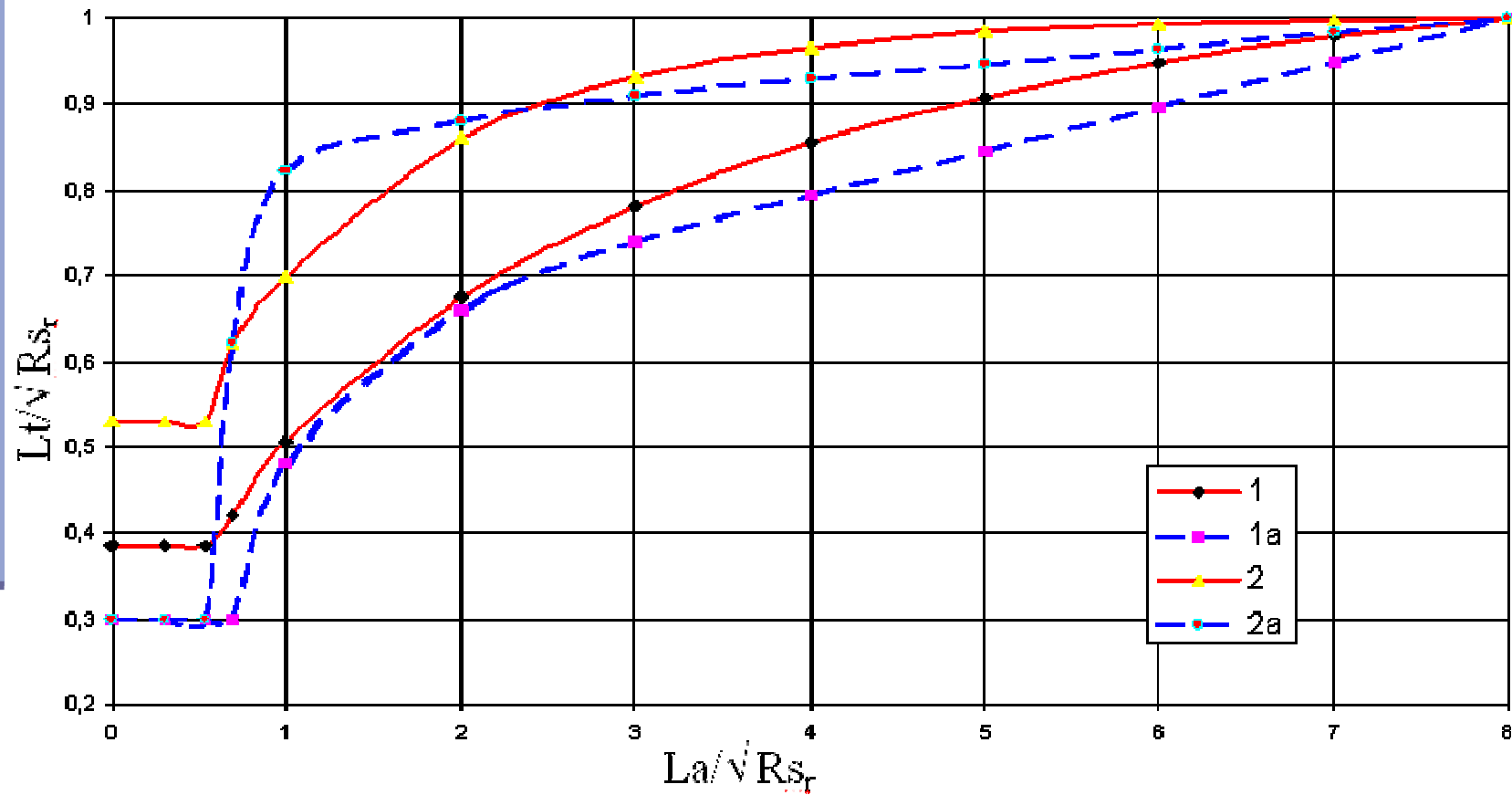


*Permissible Depth and Length of Local Thinning Area  
(fig. A)*



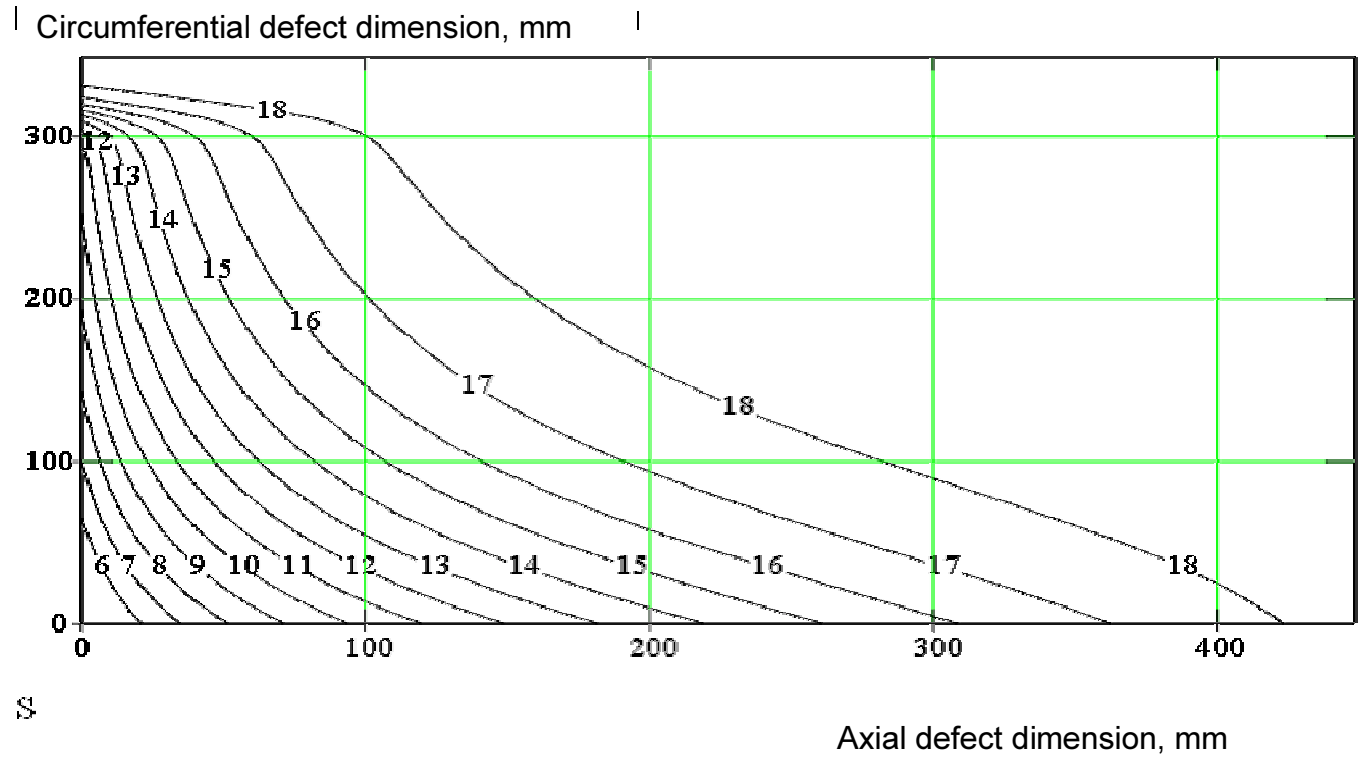
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*Comparison of Permissible Thickness Calculations by Developed Method and by Data  
 fig. A when  $L_{t1} = 1,0, \sqrt{R_s r}$ , and  $L_{t1} = 2,65\sqrt{RS}$   
 (1,2 – Guideline, 1a, 2a –data fig. A)*



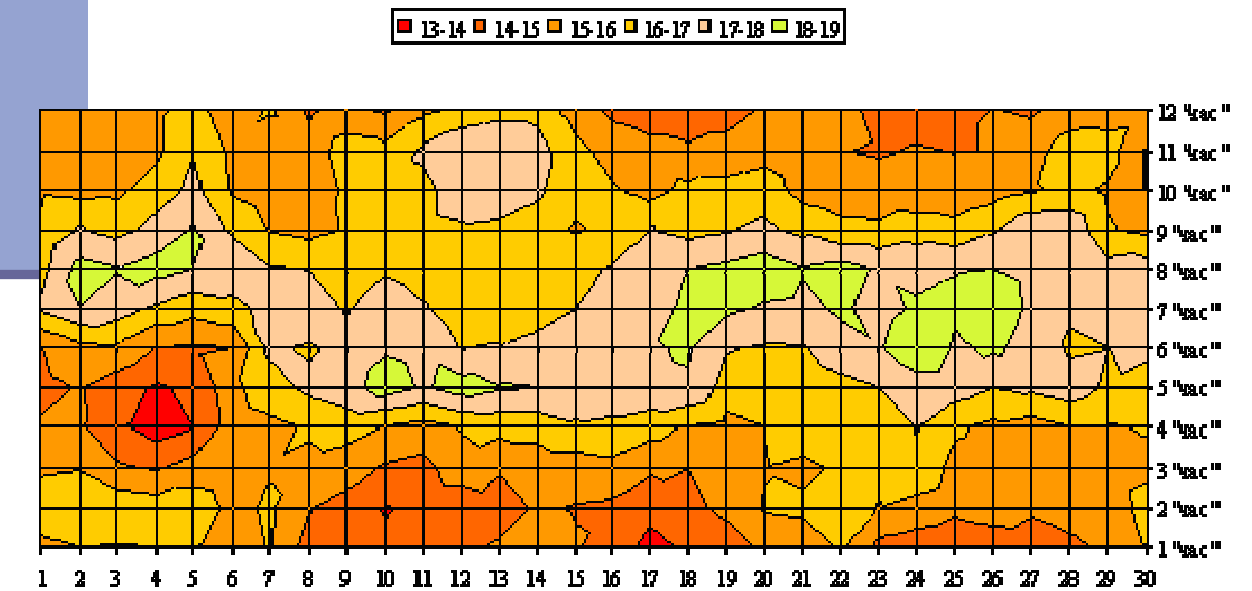
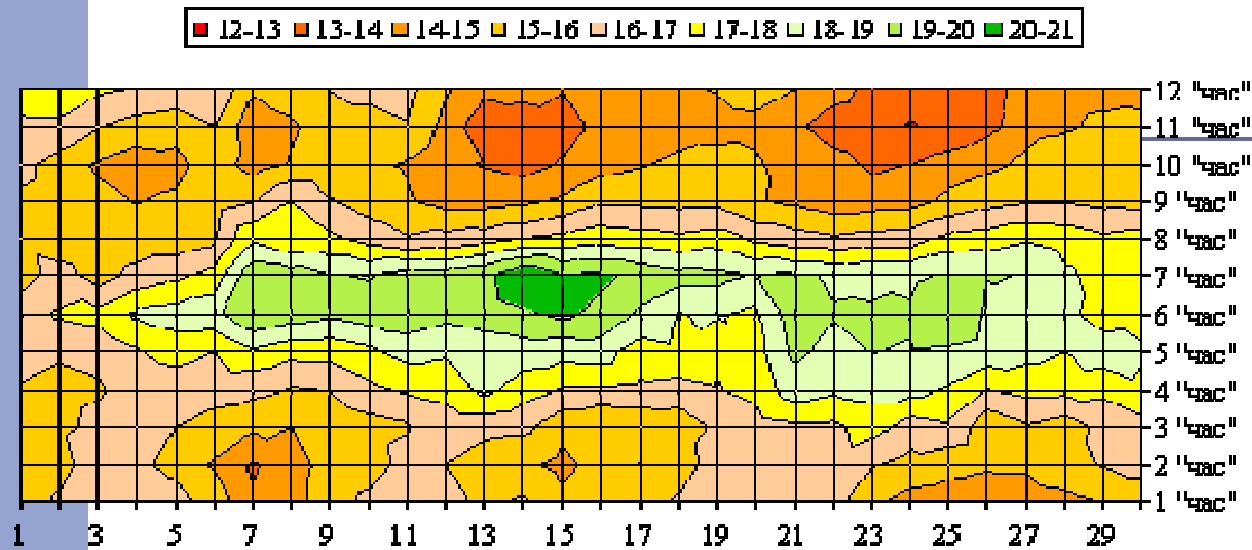
Graphs Defining the Values for Permissible Thickness of Pipelines with 530x28 mm Diameter

Initial data						Calculated values			
Steel type	Outer diam., $D_a$ ( $2R_a$ ) mm	Nom. thickn..., $s_{nom}$ , mm	Temp. $t$ , °C	Inner press..., $p$ , MPa	Add. stress $[\sigma]$ , MPa	Calc. thickn., $s_R$ mm	$L_{ct} = 0.25\pi D_a$ mm	$\sqrt{R_a s_R}$ mm	$L_{ca} = 8\sqrt{R_a s_R}$ mm
20	530	28	230	12,0	130,67	23,3	416,26	76,4	611,4




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Axial defect dimension, mm

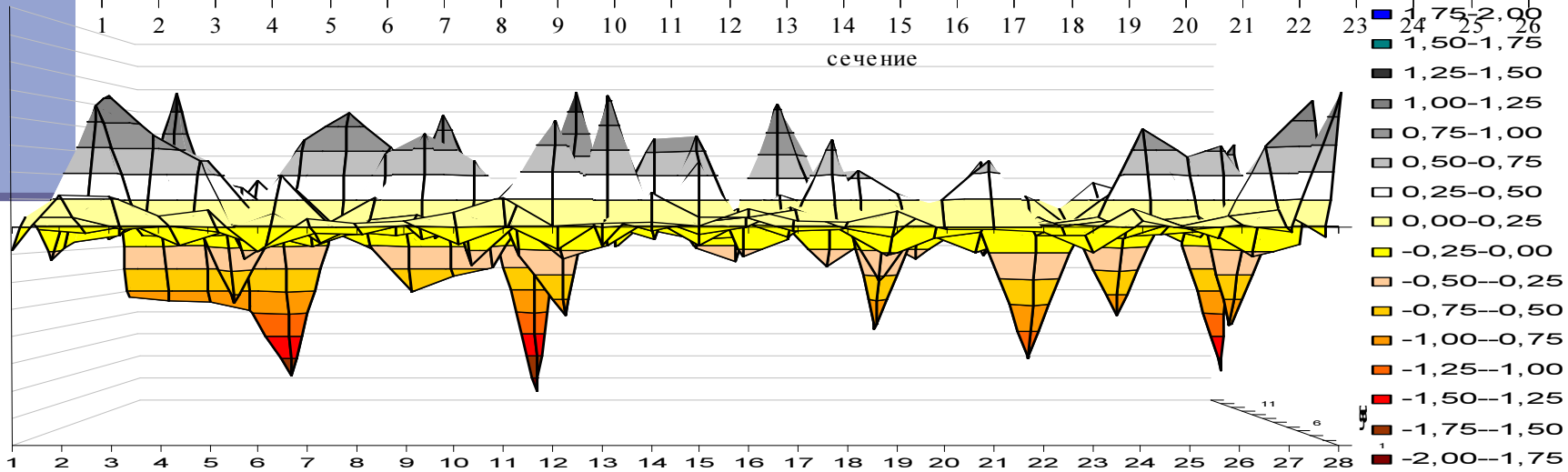
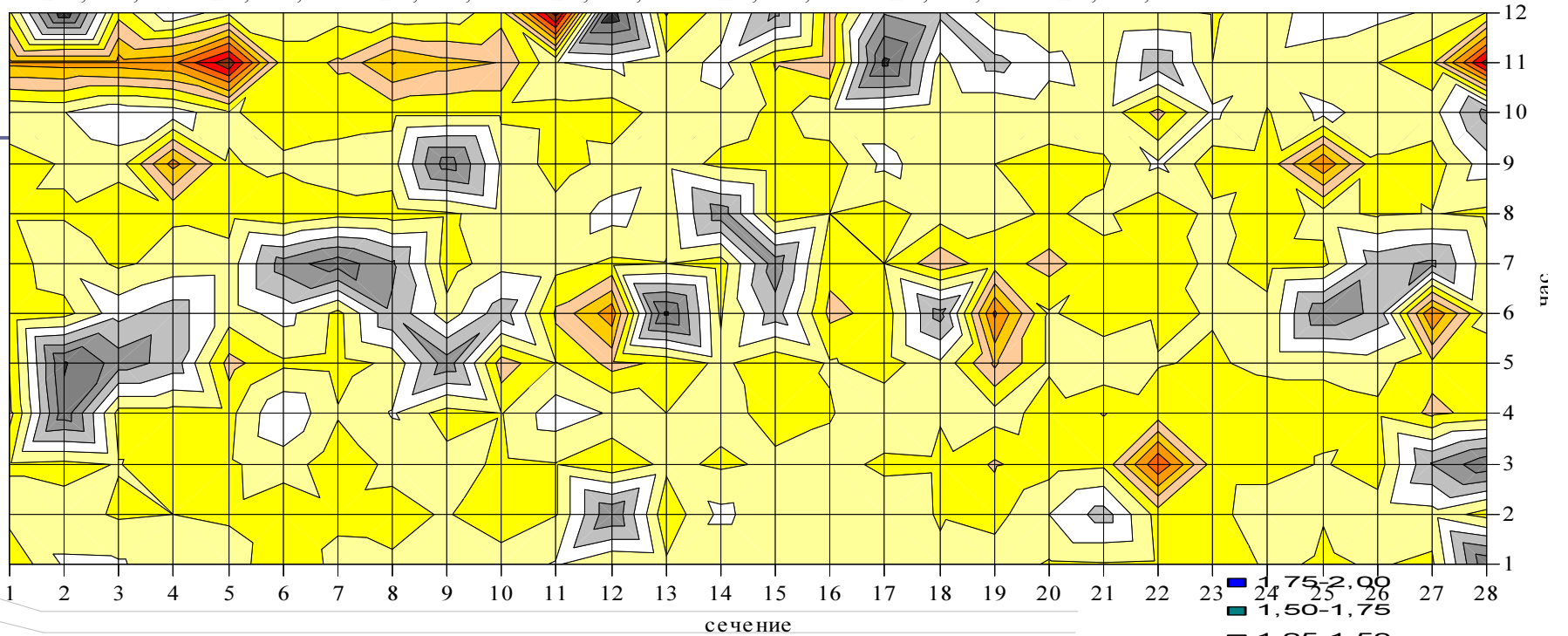
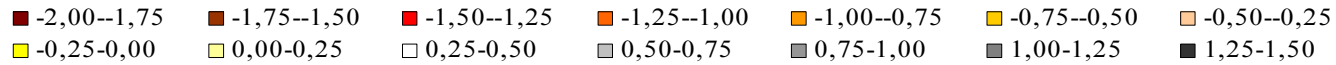


**Distribution scanning of 06-K elbow wall thickness (1996 and 2002, top and bottom correspondingly)**



# Influence of Corrosion Products Deposits on Reliability of Wall Thickness Measurements During Operating Inspections

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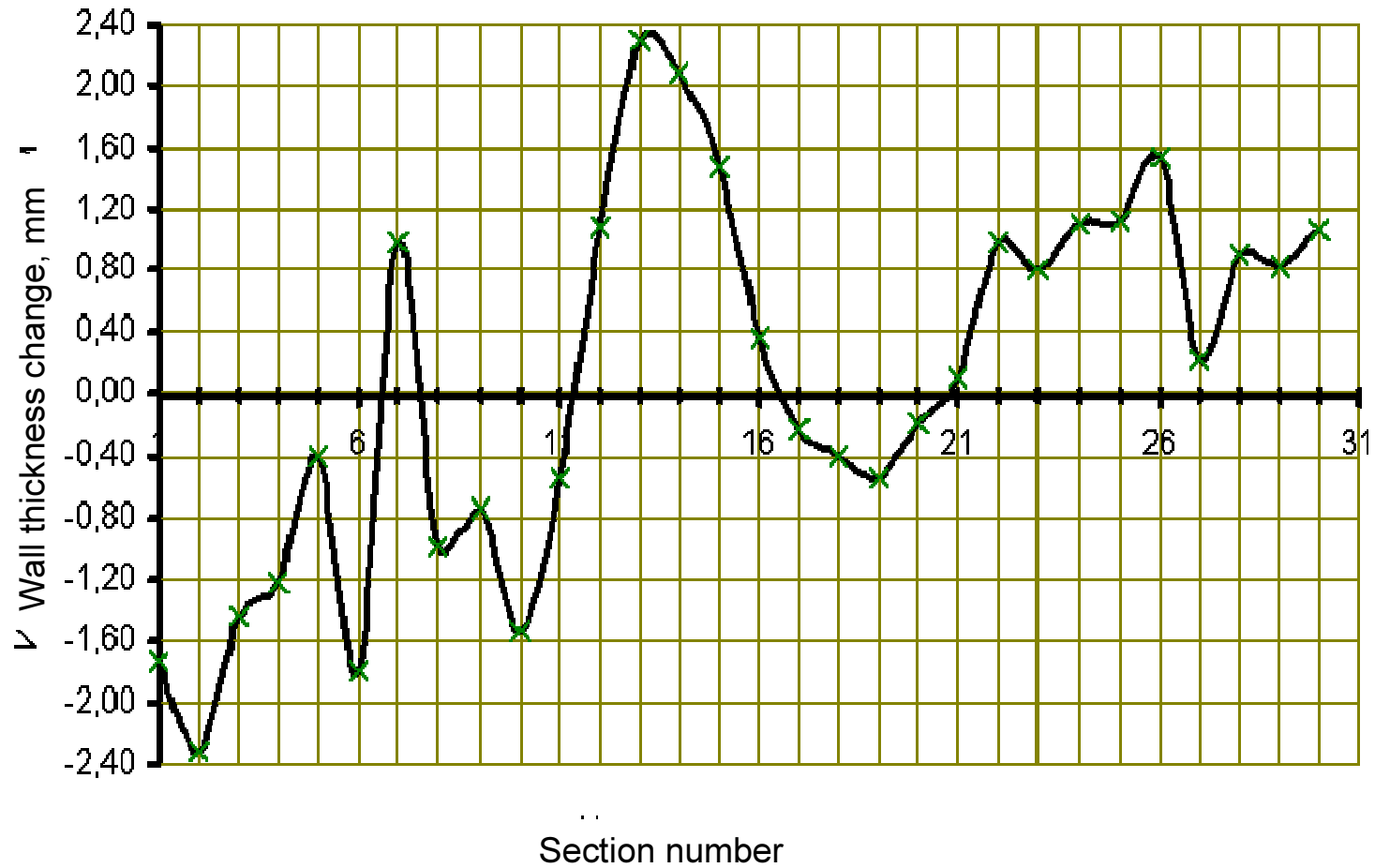
1 Distribution of thickness change between 1996 and 2000 measurements ax

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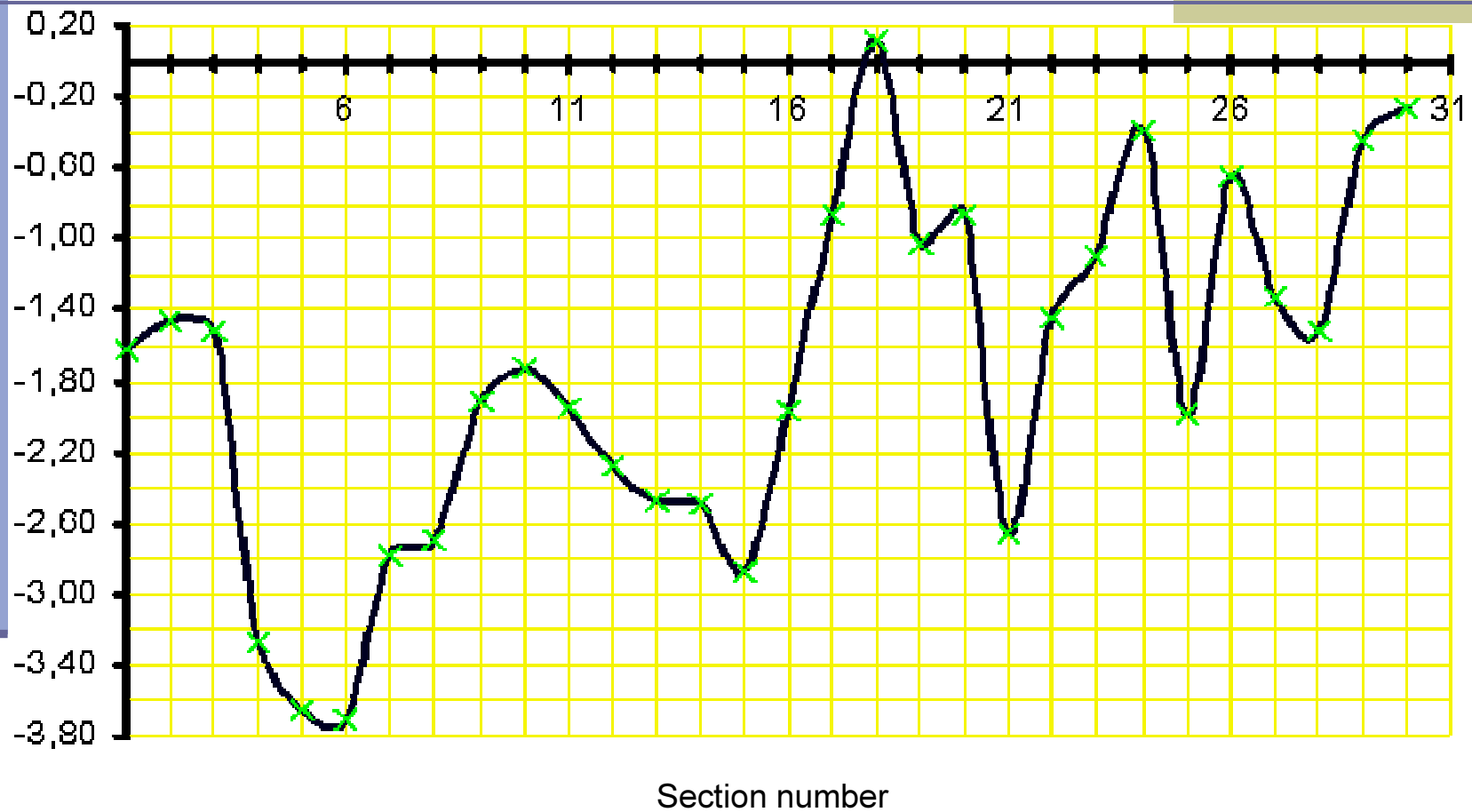
### *Date and Number of Measurements, Minimum and Maximum Values for Each Thickness Elbow, Thickness Difference, Range of Elbow Wall Thickness Change in Different Sections of Feedwater Pipeline with 465x16 mm diameter*

Elbow N	Date of meas.	Number		Values, mm			Thickness difference range. In different «hours», mm
		Section	Meas.	S <sub>мин</sub> , mm	S <sub>макс</sub> , mm	ΔS, mm	
Elbow A	1996	31	372	12,96	20,86	7,90	1,8 – 3,6
Elbow A	2002	30	360	13,50	18,72	5,23	1,6 – 2,3
Elbow Б	1995	33	394	13,84	19,94	6,10	1,9 – 2,1
Elbow Б	1996	29	342	13,95	20,13	6,18	2,1 – 2,2
Elbow Б	2000	29	348	13,76	20,12	6,37	2,2 – 2,6
Total, average value		231	2964	13,40	19,83	6,43	1,9 – 2,6

*Wall Thickness Behavior of Ø 465x16 mm Pipeline Elbow within the Period from 1996 to 2002 in 12<sup>th</sup> «hour»*



*Wall Thickness Behavior of Ø 465x16 mm Pipeline Elbow within the Period from 1996 to 2002 in 6th «hour»*



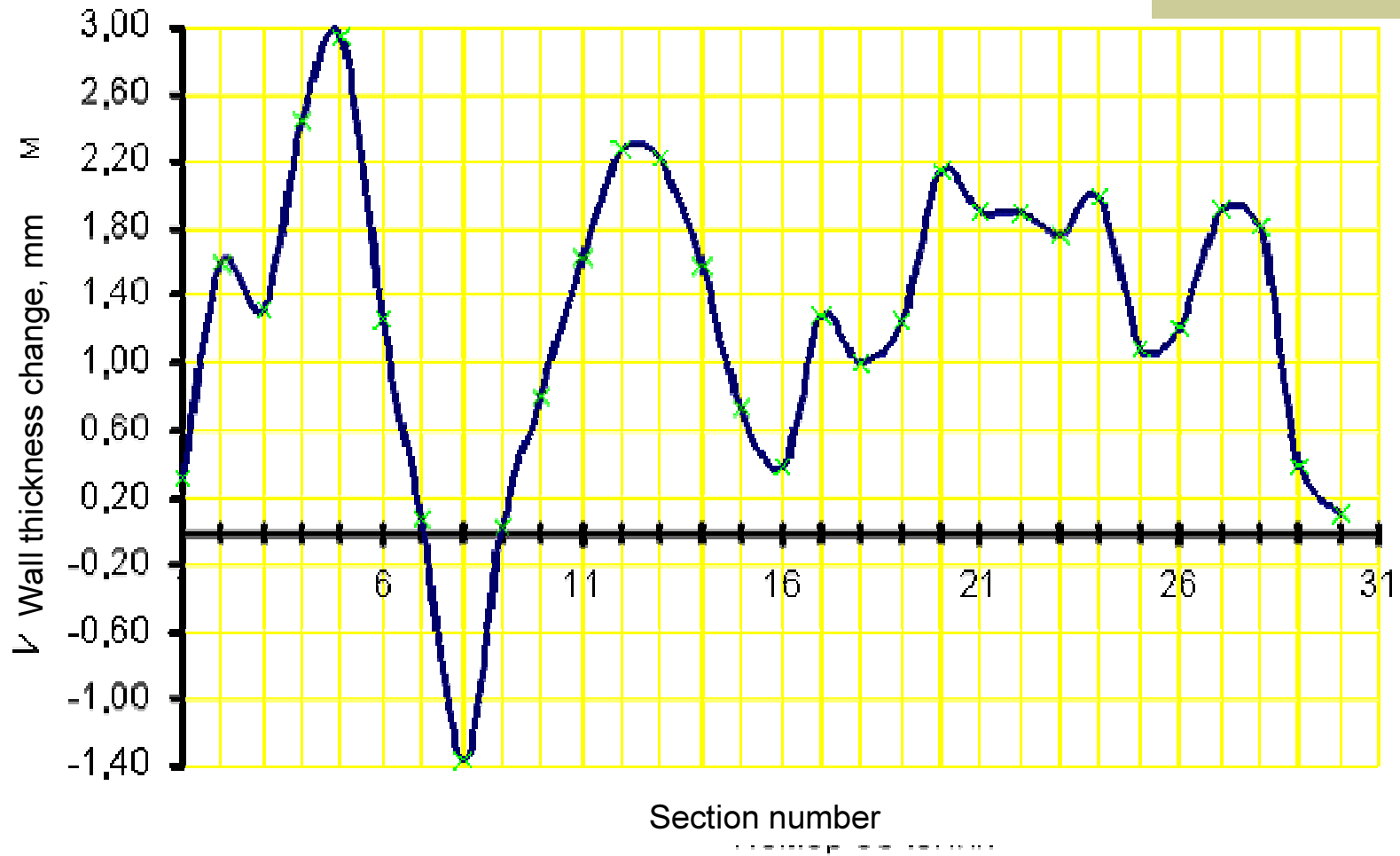
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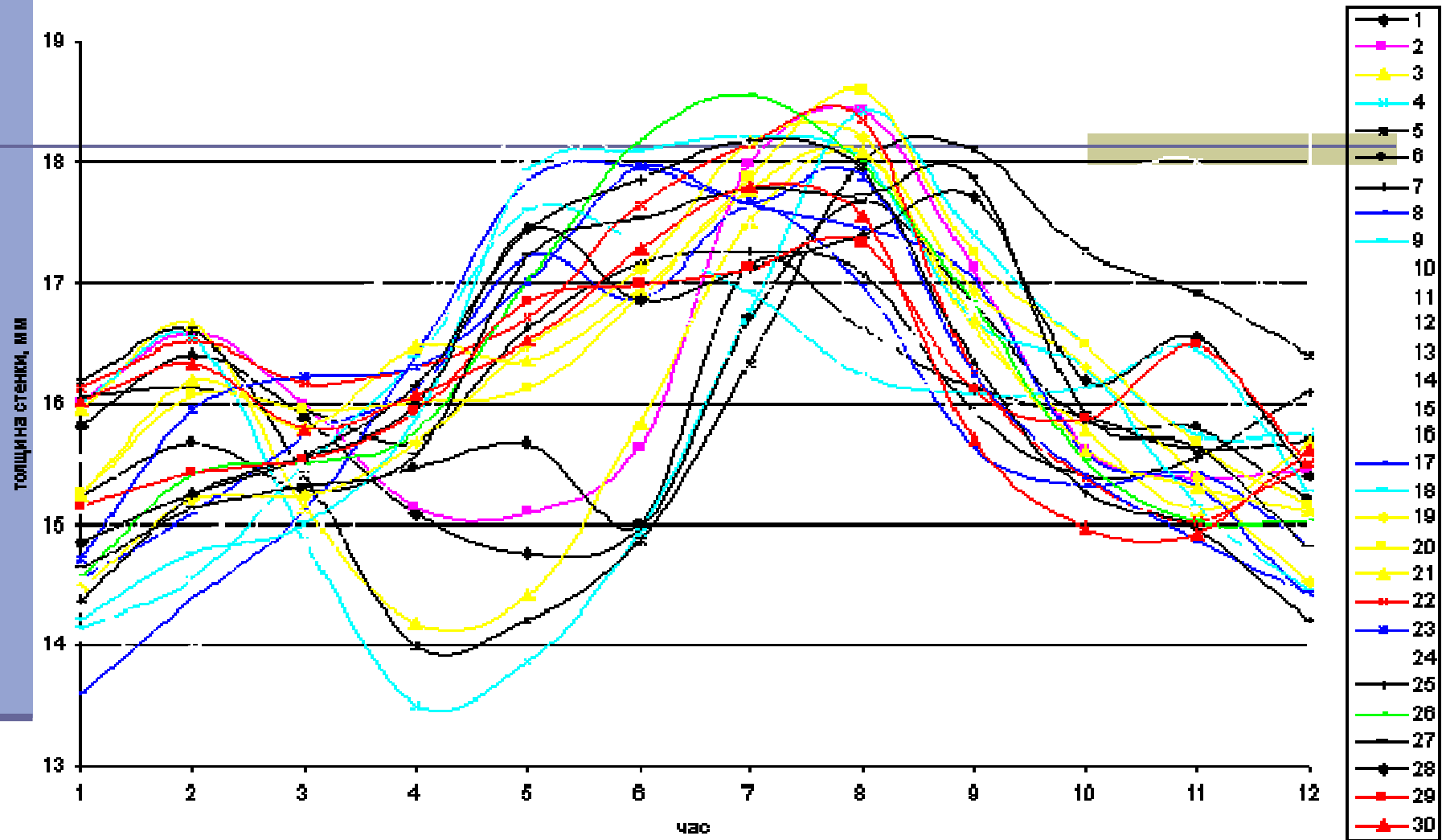
**Wall Thickness Behavior of Ø 465x16 mm Pipeline Elbow within the Period from 1996 to 2002 in 3<sup>rd</sup> «hour»**



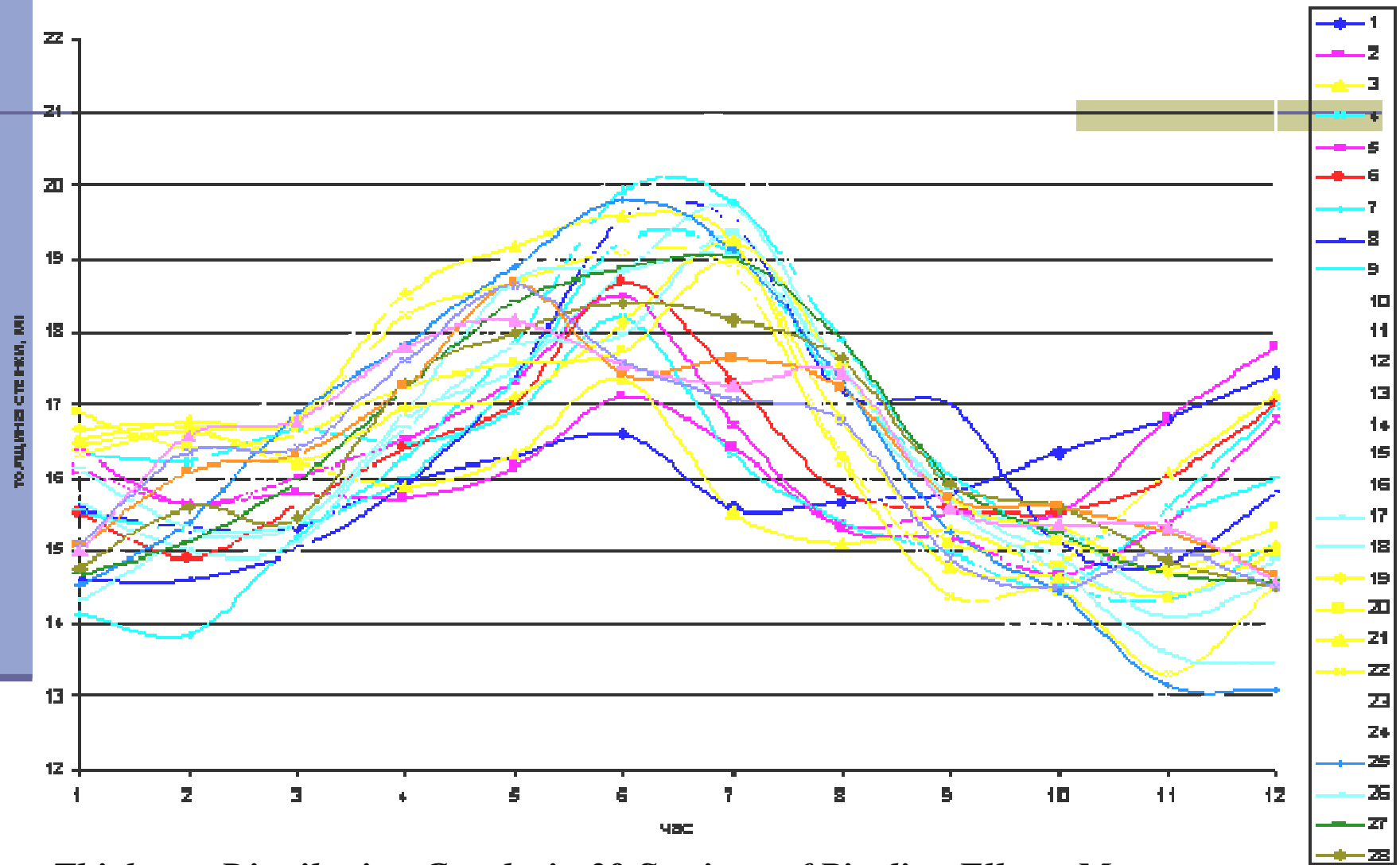
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## Analysis of Wall Thickness Behavior of Ø 465x16 mm Pipeline Elbow within the Period from 1996 to 2002 in 9th «hour»





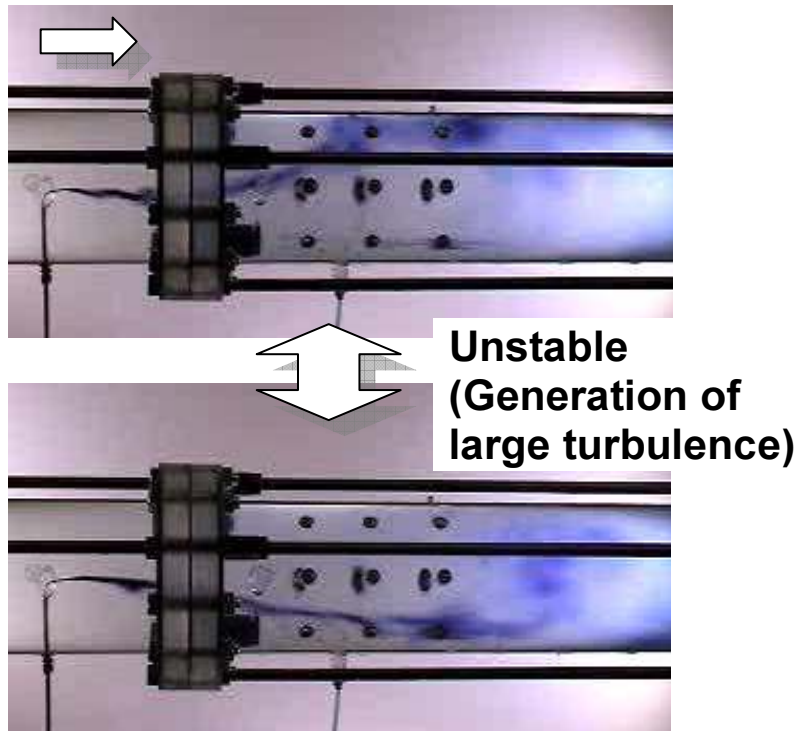
*Thickness Distribution Graphs in 30 Sections of Pipeline Elbow. Measurement of 11.09.2002, Ø 465x16 mm*



*Thickness Distribution Graphs in 29 Sections of Pipeline Elbow. Measurement of 11.09.96, Ø 465x16 mm*

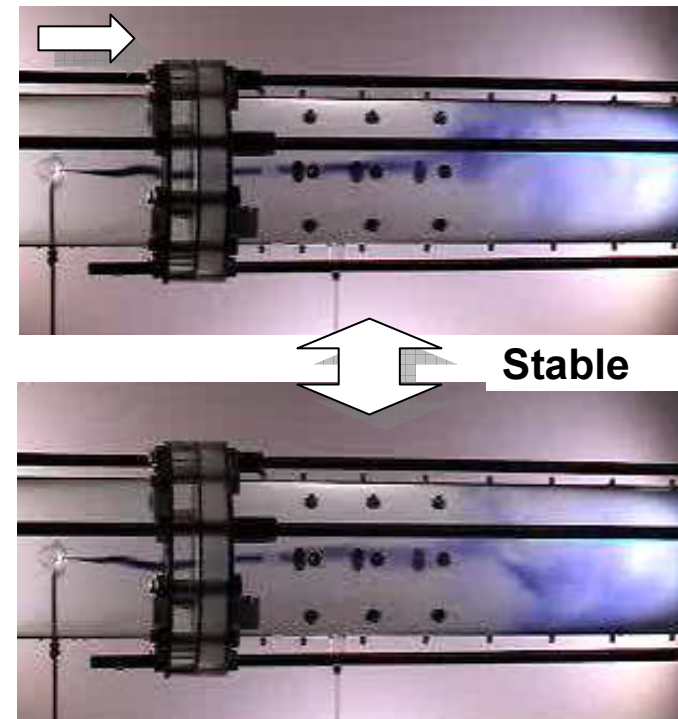
## Turbulent Flow Downstream of Orifice (Mihama)

### A-train



- Generation of relatively strong turbulence
- Unstable position of flow axis
  - Faster circumferential flow velocity than B-train

### B-train

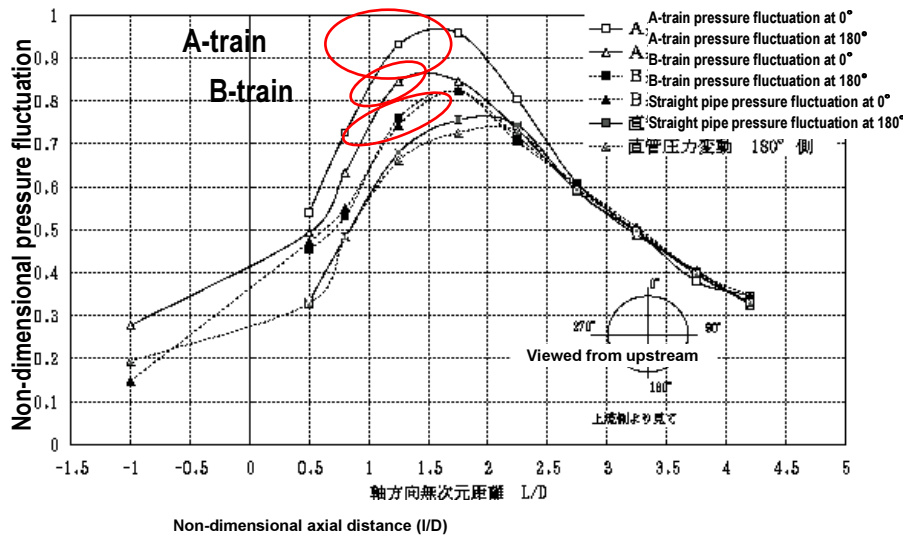


- Generation of relatively weak turbulence
- Stable position of flow axis
  - Slower circumferential flow velocity than A-train

Analytical result also shows that turbulence appeared in A-train is larger than that in B-train. <sup>24</sup>

# Distribution of Pressure Fluctuation (Mihama)

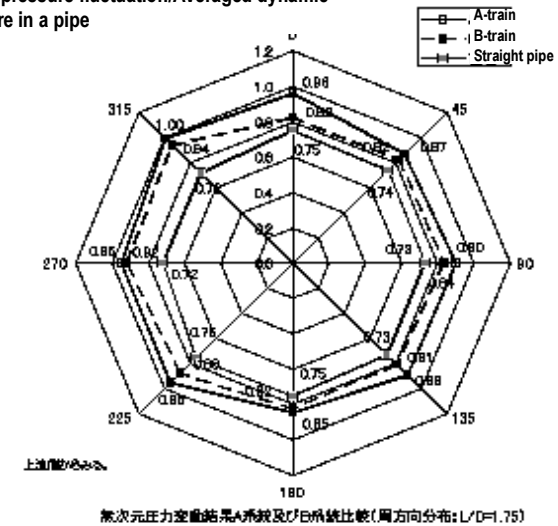
Distribution of Axial Pressure Fluctuation



Distribution of Non-dimensional pressure fluctuation (Comparison between A-train and B-train)

Distribution of Circumferential Pressure Fluctuation

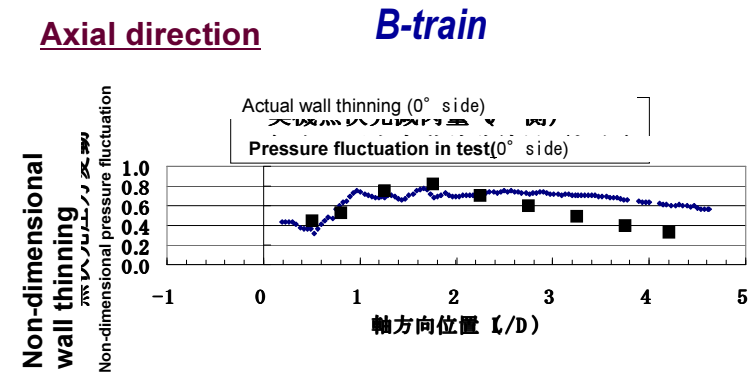
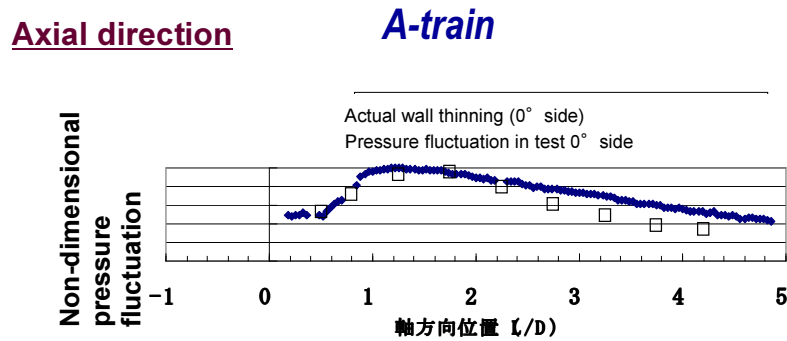
Non-dimensional pressure fluctuation = RMS of pressure fluctuation/Averaged dynamic pressure in a pipe



Comparison of non-dimensional pressure fluctuations between A-train and B-train (circumferential distribution at L/D = 0.8)

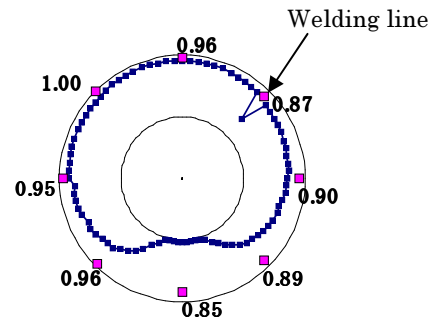
- Degree of pressure fluctuation: A-train > B-train > Straight pipe
- Characteristics of A-train: Pressure fluctuations at 0° is larger than 180°
- Characteristics of B-train and straight pipe: No difference between 0° and 180°

# Comparison Between Actual Wall Thinning and Visualization Test (Mihama)



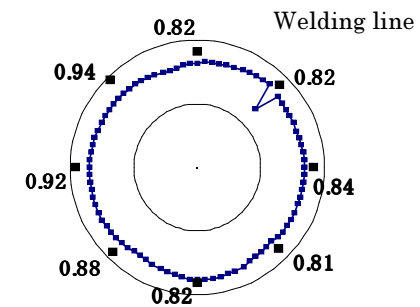
**Circumferential direction**

— Actual wall thinning (L/D 1.74)  
■ Pressure fluctuation in test L/D=1.75



**Circumferential direction**

— Actual wall thinning (L/D 1.74)  
■ Pressure fluctuation in test L/D=1.75



- Axial wall thinning: wall thinning trends at the actual plant corresponds to pressure fluctuation trends in visualization test.
- Circumferential wall thinning: wall thinning trends at the actual unit (A>B) corresponds to pressure fluctuation trends in visualization test (A>B).

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## Conclusions

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1. The set of normative documents on calculation of erosion-corrosion wear has been developed including software tools, guidelines on calculations of permissible thickness for pipeline elements, guidelines on establishing chemical composition of pipeline metal
2. Application of normative documents provides for optimization of operating inspection scope and frequency, evaluation of technical state and definition of residual life.
3. It was found that availability of corrosion products deposits influences significantly on UT measurements reliability of pipeline wall thickness.